## **ELECTRICAL RESISTIVITY SURVEY FOR GROUND WATER POTENTIALS, AN OVERVIEW**

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### **Corresponding author: Opeh. R. ABSTRACT**

**A** geophysical survey for ground water resources was carried out. This was successfully done by employing the electrical resistivity method to investigate the water table variations within the areas covered, with the application of Schlumberger arrangement. Electrical resistivity technique has its base on inserting four electrodes in the ground in which two of the electrodes are current electrodes and the other two are potential electrodes. ABEM TERRAMETER SAS 300B was the principal instrument used in this survey. This instrument measures the ground resistance and the apparent resistivity of the subsurface was calculated the data obtained was analyzed by the computation of the apparent resistivity and plotting the graph of the half electrodes spacing and the apparent resistivity. Interpretation was done by computer assisted evaluation procedure in which depths of the water table was estimated for the three VES. For VES 1, the water table was found at about 47.5m, VES 2 is about 47.0m, and VES 3 is from 61.5m.

**KEY WORDS:** Electrical resistivity, Schlumberger arrangement, apparent resistivity, VES.

## **INTRODUCTION**

The rapid growth of the population in most part of the globe has in no small measure ushered in depletion of natural resources. Against this backdrop, man has continued to strive hard to develop methods of replenishing these bounties of nature. Underground water is a ground source of water to man apart from the surface water from rainfall and streams.

 Groundwater occurs in the zone of saturation below the earth surface. This water when tapped is large enough for man to sustain life and in many areas it can be used in agricultural activities like irrigation and industrial activities. The application of geophysical principles was used to investigate the ground water of the study area. The method centers on the use of electrical resistivity for ground water exploration. They are several forms electrode arrangement that can be used in carrying out resistivity measurements. In most arrangements; both sets of electrodes are laid out along a line. The current electrodes are generally placed outside of the potential electrodes. For a better result of this project, the Schlumberger method was used in tacking the problems encountered during ground water investigation. The resistivity survey techniques involve the introduction of an artificial source of current into the ground through point electrodes. ABEM TERRAMETER SAS 300 was used by employing the Schlumberger electrode arrangement to determine resistivity.

# **Brief Geology of the Study Area**

The study was carried out in Idemli local Government Area of Anambra State, Nigeria. Covering Umunachi and Eziowelle towns. The general geology of Idemili and its environs is mainly the Nanka sand. The geologic unit that is predominant is the Nanka sand of the lower Ecocene called the Persian. The formation that is underlying the Nanka sand is the Imo-shale and the formation overlying it is the Ogwashi-Asaba formation. The thickness of Nanka sand is about 350 metres. The Imo-shale, which is directly under the Nanka sand, has a thickness of about 1000 metres.Ogwashi-Asaba formation, which is above the Nanka sand, has a thickness of about 1163 metres. Erosive forces can expose this sand in places open to erosion due to non-availability of cementing material in the area. The Nanka sand of the Anambra sedimentary basin consist of four lithologic units of crossed stratified medium to coarse, often pebbly loose sand beds with intercalating of thin gypsiferous shale by Nkisi river in the North and Ndemili river in the West. The rivers are fed by many streamlets. The survey area is located between latitude  $6^{\circ}8'N$  and  $6^{\circ}11.5'N$ , and longitudes  $6^{\circ}52.6'E$  and 6°58'E covering Umunachi and Eziowelle towns.

# **Basic Theory of Electrical Resistivity**

Consider a completely homogeneous isotropic earth layer of a uniform resistivity. From the aspect of quantitative treatment, let us consider a homogenous layer of length, L and a resistance, R through which a current I, is flowing. The potential difference across the ends of the resistance will be given by Ohm's law and;

∆ *V* = *IR* ------------------------------- (1)

The area of cross-section A, resistivity  $\ell$ , resistance R and the layer is specified by its length L from the equation below;

$$
\ell = \frac{RA}{L} \quad \text{---} \quad (2)
$$

The SI unit of resistivity is Ohm-metre (Ωm). While the conductivity is  $\sigma\!=\!\left\lfloor \frac{1}{\ell}\right\rfloor$ ⅂ L  $=\left\lceil \frac{1}{\ell} \right\rceil$  $\sigma = \left| \frac{1}{a} \right|$  of a material can be defined as the reciprocal of resistivity and is measured in Ohm per metre ( $Ωm<sup>-1</sup>$ ) the

word "mho" being carried by spelling "Ohm" backward ( *Sharma*,*P*.*V*.1976 )

Therefore, it follows that  $R = \ell L/A$  and equation 1 can be rewritten as

$$
\frac{\Delta V}{I} = \frac{\ell L}{A}
$$

where *j* is the current density per unit of cross-sectional area and grad V is the potential gradient. Consider a semi-infinite conducting layer of uniform resistivity bounded by the ground surface and assume a current of strength  $+1$  entering at point  $C_1$  on the ground surface as shown below



Fig.1: Shows a method of calculating potential distribution due to a current source in a homogeneous medium The current density j, at a distance r, away from the current source, would be:

$$
j = \frac{I}{2\pi r^2} --- \infty - a
$$
  

$$
-\frac{dv}{dr} = \ell j --- \infty - b
$$

The potential gradient associated with the Current is given in equation (1.3). Now lets substitute j in equation 1.4a. Into equation 1.4b. We then have that l

6 2 2 = − *r I dr dv* π

The potential at distance r in fig. 1 can be obtained by integrating equation (6)

7 2 2 2 1 2 ∴ = − − − − − − − − − − − − − = − − = − − ∫ ∫ *r I v r I v <sup>r</sup> dr <sup>I</sup> dv* π π π l l l

The above equation 7 can be said to be the basic equation, which enables the calculation of the potential distribution in a homogeneous conducting semi-infinite medium. It is also easy to see from equation (7) that the potential difference between points  $P_1$  and  $P_2$  (fig 1 caused by current  $+1$  at the "source" entry point  $C_1$ ) is given as:

$$
v = \frac{I\ell}{2\pi} \left[ \frac{1}{C_1 P_1} \right] - \frac{I\ell}{2\pi} \left[ \frac{1}{C_1 P_2} \right]
$$

$$
v = \frac{I\ell}{2\pi} \left[ \frac{1}{C_1 P_1} - \frac{1}{C_1 P_2} \right] - \dots - \dots - 8
$$

In the same manner, the potential difference between  $P_1$  and  $P_2$  is

$$
v = \frac{I\ell}{2\pi} \left[ \frac{1}{C_2 P_1} - \frac{1}{C_2 P_2} \right] - \dots - \dots - 9
$$

The total potential difference between  $P_1$  and  $P_2$  is therefore, given by the sum of the right hand sides of equation (1.7) and (1.8) which is:

$$
v = \frac{I\ell}{2\pi} \left[ \frac{1}{C_1 P_1} - \frac{1}{C_1 P_2} \right] - \frac{I\ell}{2\pi} \left[ \frac{1}{C_2 P_1} - \frac{1}{C_2 P_2} \right]
$$
  

$$
v = \frac{I\ell}{2\pi C_1 P_1} - \frac{I\ell}{2\pi C_1 P_2} - \frac{I\ell}{2\pi C_2 P_1} + \frac{I\ell}{2\pi C_2 P_2}
$$

Collecting like terms

$$
v = \frac{I\ell}{2\pi} \left[ \frac{1}{C_1 P_1} - \frac{1}{C_1 P_2} - \frac{1}{C_2 P_1} + \frac{1}{C_2 P_2} \right] - \dots - \dots - 10
$$
  
or

$$
\ell = 2\pi G \frac{\Delta v}{I} (Sharma, P.V.1976) \quad - \quad - \quad - \quad - \quad - \quad - \quad 11
$$

Where:

$$
G = \left[ \frac{1}{C_1 P_1} - \frac{1}{C_1 P_2} - \frac{1}{C_2 P_1} + \frac{1}{C_2 P_2} \right]^{-1}
$$

G denotes the geometric factor of an electrode configuration.

Here, the value of  $\ell$  for a homogeneous conducting medium is independent of the positions of electrodes and is not affected when the positions of the current and potential electrodes are interchanged.

## **METHODOLOGY**

The method applied for this research work is the vertical electrical sounding (VES) method, which is also known as electrical drilling or expanding probe. For this work three sounding points were occupied using the Schlumberger array method with the electrode spacing varying from 1.5m to about 370m and it helps in showing the multi-layered sub-surface.



Fig 2: The current was fed into the ground using two current electrodes A & B spaced at a distance AB apart as shown in fig 2 above. At the centre of these two electrodes the voltage, was measured between the potential electrodes M & N placed at a distance of MN apart. The ABEM TERRAMETER has a high resolution and gives a direct readout of the resistance of the ground in Ohms. A maximum current electrode separation (AB) of 370m was used on both sides and the corresponding potential electrodes (MN) was occasionally expanded from 0.5m to 14.0m for VES 1 & VES 3for greater depth penetration. The readings of the resistance were converted to apparent resistivity by using the expression below:

$$
\ell_a = \frac{\pi \left[ \left( \frac{AB}{2} \right)^2 - \left( \frac{MN}{2} \right)^2 \right] R}{MN}
$$

**Where** 

 $l_a$  = apparent resistivity

 $R =$  ground resistivity

AB = separation between current electrodes

MN = separation between potential electrodes.

Therefore, we can define the VES method as the use of electrical methods with depth control in which electrode spacing is increased to obtain information from greater depths at a given surface location. It is used for detecting changes in the resistivity of the earth with depth beneath the given location. The principles of VES are based on the fact that the wider the current electrode separation, the deeper the current penetration. As the current reaches greater depths subsequent readings are progressively taken

## **RESULTS & DISCUSSIONS**

A field survey was conducted through the vertical electrical sounding (VES). The data obtained from the measurement are represented in table a, b and c for VES 1, 2 and 3 respectively.





## **TABLE A FOR VES 1**





### **TABLE B FOR VES 2**



# **TABLE C FOR VES 3**

The graphs below represent VES 3, VES 2, and VES 1 in that order. (OB 3, OB 2, OB 1 respectively)

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Geo-electric section of VES 2 (not to scale)



Geo-electric section of VES 3 (not to scale)





## **COMPUTER PROGRAM ANALYSIS**

The qualitative interpretation of geo-electrical sounding data for the purpose of this work involves mainly direct computer interpretation. This is very useful in the determining the thickness and corresponding resistivity of various layers. The data from these sounding stations were sent to the computer for analysis and interpretation. From the information gotten, the stratigraphic properties of the various layers were deduced.

## **GEOELECTRIC SECTION ANALYSIS**

From VES 1, the first layer is about 0.6m thick and it represents the top soil. The second layer is about 27.7m thick and it consists of laterite with a resistivity of about 384Ωm. The last layer Has a resistivity of about 2430 Ωm and it is the electric basement zone. From VES 2, the first layer is about 0.8m thick and it represents the top soil and its resistivity is about 146 Ωm. The thickness of the second layer is about 32.8m and it consists of laterite. The third layer is made up of coarse sand and has a high resistivity of about 3660 Ωm. the fourth layer is made up of medium coarse sand. This layer is a potential aquifer layer with respect to available lithological logs of boreholes already drilled in the area And from VES 3, the first layer represents the top soil and is about 0.7m thick and its resistivity is about 1210Ωm. The thickness of the second layer is about 12.3m and it is made up of laterite soil. The third layer is made up of coarse sand and is about 48.5m thick. And the fourth layer contains medium coarse sand has a high resistivity of about 10800Ωm. This is the aquifer unit.



The results are summarized in the table below:

**TABLE D: Showing the Resistivity and Depths of the Various Depths of Interest** 

Given the table above, VES 1 has the lowest resistivity of  $543Ωm$  with the depth of water table at about 47.5m.This VES has a higher potential for water. Water bearing zones always have a low resistivity. So it is advisable to sink boreholes in the areas such as VES 1. VES 1& 2 have a lower quantity of water as can be seen from their very high resistivities. So, for the purpose of sinking boreholes, the drilling should be done up to 57m in areas such as VES 1.

## **CONCLUSION**

Three vertical electrical sounding was conducted to acquire information on the hydro geological potentiality of the areas. Computer program was employed for the interpretation of the results from the field. The results of aquiferous zones and depth of each sounding stations can really help in borehole sitting in the study area. Ability to select priority areas for ground water development by the use of resistivity sounding measurements bring about a substantial reduction in exploration costs by the number of drill holes made to obtain groundwater information. The good correlation with available borehole data justified the usefulness of the method as a first approach in solving groundwater problems or for planning groundwater development programmes. The depth of water tables in the area surveyed varies from 47.5m to 61.5m.

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